IN THE SPECIFICATION

Please replace the paragraph beginning at page 25, line 5 through page 26 line 10, with the following paragraph:

-- More specifically, the delivery pressures of the hydraulic pumps 1, 2 and the control pressure from the solenoid control valve 32 are introduced respectively to pressure bearing chambers 22a, 22b and 22c of an operation drive sector. When the sum of hydraulic forces of the delivery pressures of the hydraulic pumps 1, 2 is smaller than a value of the difference between a resilient force of a spring 22d and a hydraulic force of the control pressure introduced to the pressure bearing chamber 22c, a valve member 22e is moved to the right, as viewed in Fig. 1, such that the pilot pressure from the pilot pump 9 is transmitted to the pressure bearing chamber 20d without being reduced, to thereby increase the tilting of each hydraulic pump 1, 2. As the sum of hydraulic forces of the delivery pressures of the hydraulic pumps 1, 2 is increased in excess of the above-mentioned difference value, the valve member 22a 22e is moved to the left, as viewed in Fig. 1, such that the pilot pressure from the pilot pump 9 is transmitted to the pressure bearing chamber 20d after being reduced, to thereby reduce the tilting of each hydraulic pump 1, 2. As a result, the tilting (displacement) of each hydraulic pump 1, 2 is reduced corresponding to a rise of the delivery pressures of the hydraulic pumps 1, 2, and the maximum absorption torque of the hydraulic pumps 1, 2 is controlled so as to not exceed a setting value. At that time, the setting value of the maximum absorption torque is decided by the

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value of the difference between the resilient force of the spring 22d and the hydraulic force of the control pressure introduced to the pressure bearing chamber 22c, and the setting value is variable depending on the control pressure from the solenoid control valve 32. When the control pressure from the solenoid control valve 32 is low, the setting value is large, and as the control pressure from the solenoid control valve 32 rises, the setting value is reduced.--

Please replace the paragraph beginning at page 34, line 18 through page 35, line 1 with the following paragraph:

-- The output pressure computing section 70i 70j receives the maximum absorption torque TR and computes an output pressure (control pressure) SP3 for the solenoid control valve 32 at which the setting value of the maximum absorption torque decided depending on the difference between the force of the spring 22d and the hydraulic force in the pressure bearing chamber 22c of the second servo valve 22 becomes TR. The solenoid output current computing section 70n computes the drive current SI3 for the solenoid control valve 30 32 at which the output pressure (control pressure) SP3 is obtained, and then outputs the drive current SI3 to the solenoid control valve 32.--

Please replace the paragraph beginning at page 45, line 17 through line 25, with the following paragraph:

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--   The limiter computing sections 700u gives a limiter, which limits a maximum revolution speed and a minimum revolution speed specific to the engine, to the target engine revolution speed NRO1, thereby computing the target engine revolution speed NR1 that is sent to the fuel injector 14 (see Fig. 1). The target engine revolution speed NR1 is also sent to the pump maximum absorption torque computing section ~~70e~~ 70i (see Fig. ~~6~~7) in the controller 70, which is related to the control of the hydraulic pumps 1, 2.--

         Please replace the paragraph beginning at page 51, line 28 through page 52, line 16, with the following paragraph:

--   Further, the functions of the pump maximum absorption torque computing section 70i, the output pressure computing section 70j and the solenoid output current computing section ~~70j~~ 70h of the controller 70, shown in Fig. 7, as well as the solenoid control valve 32 and the pressure bearing chamber 22c of the second servo valve 22 constitute maximum absorption torque modifying means for modifying the setting value to increase the maximum absorption torque of the hydraulic pump 1, 2 when the target revolution speed is modified to be lower than the preset rated revolution speed (i.e., the maximum rated revolution speed Nmax) by the first modifying section (i.e., the engine-revolution-speed modification gain computing sections 700d1-700d6, the minimum value selecting section 700e, the hysteresis computing section 700f, the engine-revolution-speed modification amount computing

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section 700g, and the first reference target engine-revolution-speed modifying section 700h).--

Please replace the paragraph beginning at page 62, line 5 through line 24, with the following paragraph:

--   (4) The pump control section shown in Fig. 7 operates such that, when the target delivery rates QR11, QR21 of the hydraulic pumps 1, 2 computed in the reference pumping rate computing sections 70a, 70b and the target pumping rate computing sections 70c, 70d are varied with changes of the control pilot pressures PL1, PL2 of the hydraulic pumps 1, 2 due to changes of the operation pilot pressures, the target delivery rate rates QR11, QR21 are is divided by the actual engine revolution speed NE1 in the target pump tilting computing sections 70e, 70f to obtain the target tiltings θR1, θR2. Therefore, the delivery rates of the hydraulic pumps 1, 2 are provided as flow rates depending on the target delivery rate rates QR11, QR21. Even if a response is delayed in the control of the engine revolution speed when there occurs a difference between the target revolution speed NR1 and the actual revolution speed NE1 of the engine 10, the delivery rates of the hydraulic pumps 1, 2 can be controlled with a good response depending on the changes of the operation pilot pressures (i.e., the changes of the target delivery rates QR11, QR21), and superior operability can be obtained.--